

Three Level Designs

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Three Level Designs

In this session, we will discuss:

- Types of Input Factors: Qualitative versus Quantitative
- KISS Guidelines Flowchart
- Three Level Designs
 - Full Factorial (3^k Designs)
 - ⁻ L₁₈ Screening Designs
 - Response Surface Modeling Designs
 - Box Behnken Design
 - Central Composite Design (CCD)



- A list of supplemental material and additional practice/review questions for this session are provided at the end of this presentation
- You can download the pdf of this presentation, along with any supporting data files, on the site where you are accessing this course



Input Factor Types and Levels

- Types of Input Factors
 - Qualitative (Input factor significance)
 - Quantitative (Models!)
 - Mixed factors (Both)
- Number of levels for each input factor
 - Two levels
 - Three levels
 - Mixed levels







Y-hat Surface Plot

KISS Guidelines for Choosing an Experimental Design



NOTE 1: Sample size (n_{reps}) is for 95% confidence in \hat{s} and 99.99% confidence in \hat{y} .

NOTE 2: $(n_{reps}/2)$ will provide 75% confidence in \hat{s} and 95% confidence in \hat{y} .

NOTE 3: The 12 Run Plackett-Burman or L12 is very sensitive to large numbers of interactions. If this is the case, you would be better off using the 16 Run Fractional Factorial or a smaller number of variables in 2 or more full factorial experiments.

NOTE 4: For more complete 2-level design options, see next page.



DOE PRO XL Three Level Designs

DOE PRO XL follows the KISS Guidelines!

• DOE PRO XL > Create Design > Computer Aided ...







KISS Guidelines for Choosing and Experimental Design



NOTE 2: $(n_{rens}/2)$ will provide 75% confidence in \hat{s} and 95% confidence in \hat{y} .

NOTE 3: The 12 Run Plackett-Burman or L12 is very sensitive to large numbers of interactions. If this is the case, you would be better off using the 16 Run Fractional Factorial or a smaller number of variables in 2 or more full factorial experiments.

NOTE 4: For more complete 2-level design options, see next page.



Three Level Full Factorial Designs

OBJECTIVE: To test all possible combinations $(n = 3^k)$

ADVANTAGES: Can estimate all mains, all quadratics, and all linear interactions. Can mix qualitative and quantitative factors.

DISADVANTAGES: Very costly when k > 3. Very inefficient due to sparsity of high-order interactions.



Full Factorial Design Space

| Factors | | | 1 | Factors | | | 1 | Factors | | | |
|---------|---|----|----|---------|---|----|----|---------|----|----|----|
| Run | А | в | С | Run | Α | в | С | Run | Α | в | С |
| 1 | 1 | 1 | 1 | 10 | 0 | 1 | 1 | 19 | -1 | 1 | 1 |
| 2 | 1 | 1 | 0 | 11 | 0 | 1 | 0 | 20 | -1 | 1 | 0 |
| 3 | 1 | 1 | -1 | 12 | 0 | 1 | -1 | 21 | -1 | 1 | -1 |
| 4 | 1 | 0 | 1 | 13 | 0 | 0 | 1 | 22 | -1 | 0 | 1 |
| 5 | 1 | 0 | 0 | 14 | 0 | 0 | 0 | 23 | -1 | 0 | 0 |
| 6 | 1 | 0 | -1 | 15 | 0 | 0 | -1 | 24 | -1 | 0 | -1 |
| 7 | 1 | -1 | 1 | 16 | 0 | -1 | 1 | 25 | -1 | -1 | 1 |
| 8 | 1 | -1 | 0 | 17 | 0 | -1 | 0 | 26 | -1 | -1 | 0 |
| 9 | 1 | -1 | -1 | 18 | 0 | -1 | -1 | 27 | -1 | -1 | -1 |

27 Full Factorial Design Conditions for K=3







| Name, Lo | w, High Definition Windo | WC | | \times |
|-----------|------------------------------|------------------|------|-----------------|
| Enter the | e name, low, and high values | for each Factor. | | |
| Factor | Name | Low | High | <u>N</u> ext >> |
| A (3) | Supplier | 1 | 3 | << <u>B</u> ack |
| B (3) | Temp | 100 | 200 | <u>C</u> ancel |
| C (3) | Pressure | 50 | 80 | |
| | | | | <u>H</u> elp |

| Number of Replications/Responses | × |
|---|-----------------|
| How many responses do you have? | <u>N</u> ext >> |
| 1 ~ | << <u>B</u> ack |
| How many replications would you like? (Note: If using multiple responses create enough | <u>C</u> ancel |
| replications for the most demanding response.) | <u>H</u> elp |
| 3 | |



| Response Names | | \times |
|--------------------------------------|---|--------------------|
| Enter the respon for each respons | se names. You may use up to 15 characters se name. | Fi <u>n</u> ish >> |
| Response #1 | Mixing Time | << <u>B</u> ack |
| | | <u>C</u> ancel |

| Factor | Α | В | С | Mixing Tim | e | | |
|--------|----------|------|----------|-------------------|------|----------|--|
| Row # | Supplier | Temp | Pressure | Y1 | Y2 | Y3 | |
| 1 | 3 | 200 | 80 | 12 | 12 | 13 | |
| 2 | 3 | 200 | 65 | 13 | 12 | 13 | |
| 3 | 3 | 200 | 50 | 14 | 13 | 13 | |
| 4 | 3 | 150 | 80 | 15 | 15 | 16 16 | |
| 5 | 3 | 150 | 65 | 15 | 15 | 16 16 | |
| 6 | 3 | 150 | 50 | 16 | 16 | 15 | |
| 7 | 3 | 100 | 80 | 15 | 15 | 16 16 | |
| 8 | 3 | 100 | 65 | 15 | 15 | 16 16 | |
| 9 | 3 | 100 | 50 | 16 | 16 | 15 | |
| 10 | 2 | 200 | 80 | 17 | 17 | 18 | |
| 11 | 2 | 200 | 65 | 18 | 18 | 17 | |
| 12 | 2 | 200 | 50 | 19 | 19.5 | 18 | |
| 13 | 2 | 150 | 80 | 18 | 19 | 18 | |
| 14 | 2 | 150 | 65 | 20 | 21 | 20 | |
| 15 | 2 | 150 | 50 | 20 | 20 | 21 | |
| 16 | 2 | 100 | 80 | 20 | 19 | 20 | |
| 17 | 2 | 100 | 65 | 20 | 21 | 21 | |
| 18 | 2 | 100 | 50 | 21 | 21 | 22 | |
| 19 | 1 | 200 | 80 | 8 | 8 | 7 | |
| 20 | 1 | 200 | 65 | 9 | 8 | 8 | |
| 21 | 1 | 200 | 50 | 9 | 9 | 8 | |
| 22 | 1 | 150 | 80 | 10 | 9 | 9 | |
| 23 | 1 | 150 | 65 | 10 | 9 | 10 | |
| 24 | 1 | 150 | 50 | 10 | 10 | 9 | |
| 25 | 1 | 100 | 80 | 9 | 10 | 10 | |
| 26 | 1 | 100 | 65 | 10 | 11 | 10 | |
| 27 | 1 | 100 | 50 | 11 | 11 | 12 | |
| | | | | | | | |



DOE PRO XL > Analyze Design > Marginal Means Plot...









DOE PRO XL > Analyze Design > Multiple Response Regression

| Y-hat Model | | | | | |
|-------------|--------------------|--------------------|-----------|--------|-------|
| | | Mixing Time | | | |
| | | | | | , ive |
| Factor | Name | Coeff | P(2 Tail) | Tol | Act |
| Const | | 19.858 | 0.0000 | | |
| А | Supplier | 2.870 | 0.0000 | 0.2000 | X |
| В | Temp | -1.333 | 0.0000 | 0.2000 | X |
| С | Pressure | -0.75926 | 0.0001 | 0.2000 | Х |
| AB | | -0.11111 | 0.2658 | 1 | |
| AC | | 0.11111 | 0.2658 | 1 | |
| BC | | 0.01389 | 0.8888 | 1 | |
| ABC | | -0.16667 | 0.1739 | 1 | |
| AA | | -7.407 | 0.0000 | 1 | Х |
| BB | | -0.65741 | 0.0000 | 1 | Х |
| сс | | -0.04630 | 0.7419 | 1 | |
| AAB | | 0.08333 | 0.6285 | 0.3333 | |
| ABB | | -0.55556 | 0.0019 | 0.3333 | |
| AAC | | 0.47222 | 0.0076 | 0.3333 | |
| ACC | | 0.11111 | 0.5192 | 0.3333 | |
| BBC | | -0.15278 | 0.3761 | 0.3333 | |
| BCC | | 0.04167 | 0.8087 | 0.3333 | |
| | _ | | | | |
| | R ² | 0.9848 | | | |
| | Adj R ² | 0.9810 | | | |
| | Std Error | 0.5938 | | | |
| | F | 259.1617 | | | |
| | Sig F | 0.0000 | | | |

| Factor | Name | Low | High | Exper |
|--------|----------|-----|------|-------|
| А | Supplier | 1 | 3 | 2 |
| В | Temp | 100 | 200 | 150 |
| С | Pressure | 50 | 80 | 65 |

| | Multiple Response Prediction | | | | | | |
|-------------|------------------------------|--------|-------------|---------------|--|--|--|
| | | | | | | | |
| | | | 99% Confid | ence Interval | | | |
| | Y-hat | S-hat | Lower Bound | Upper Bound | | | |
| Mixing Time | 19.8580 | 0.5843 | 18.105 | 21.611 | | | |

| S-hat Model | | | | | |
|-------------|--------------------|--------------------|-----------|--------|-----|
| | | Mixing Time | _ | | |
| | | | | | ive |
| Factor | Name | Coeff | P(2 Tail) | Tol | Act |
| Const | | 0.58425 | 0.0000 | | |
| А | Supplier | 0.0000000 | 1.0000 | 0.2000 | |
| В | Temp | 0.02071 | 0.3047 | 0.2000 | |
| С | Pressure | -0.02071 | 0.3047 | 0.2000 | |
| AB | | 0.0000000 | 1.0000 | 1 | |
| AC | | 0.0000000 | 1.0000 | 1 | |
| BC | | -0.01553 | 0.1693 | 1 | |
| ABC | | 0.0000000 | 1.0000 | 1 | |
| AA | | -0.02071 | 0.1927 | 1 | |
| BB | | 0.01036 | 0.5008 | 1 | |
| СС | | 0.01036 | 0.5008 | 1 | |
| AAB | | -0.03107 | 0.1179 | 0.3333 | |
| ABB | | 0.0000000 | 1.0000 | 0.3333 | |
| AAC | | 0.03107 | 0.1179 | 0.3333 | |
| ACC | | 0.0000000 | 1.0000 | 0.3333 | |
| BBC | | -0.01553 | 0.4124 | 0.3333 | |
| BCC | | 0.01553 | 0.4124 | 0.3333 | |
| | _ | | | | |
| | R ² | 0.6058 | | | |
| | Adj R ² | -0.0250 | | | |
| | Std Error | 0.0363 | | | |
| | F | 0.9604 | | | |
| | Sig F | 0.5454 | | | |



Final Regression Model <u>DOE PRO XL > Analyze Design > Multiple Response Regression</u>

| Y-hat Model | | | | | |
|-------------|--------------------|--------------------|-----------|-----|-------|
| | | Mixing Time | | | |
| | | | | | , ive |
| Factor | Name | Coeff | P(2 Tail) | Tol | Act |
| Const | | 19.827 | 0.0000 | | |
| А | Supplier | 2.574 | 0.0000 | 1 | Х |
| В | Temp | -1.250 | 0.0000 | 1 | Х |
| С | Pressure | -0.54630 | 0.0000 | 1 | Х |
| AA | | -7.407 | 0.0000 | 1 | X |
| BB | | -0.65741 | 0.0000 | 1 | Х |
| | _ | | | | |
| | R ² | 0.9791 | | | |
| | Adj R ² | 0.9777 | | | |
| | Std Error | 0.6438 | | | |
| | F | 701.5622 | | | |
| | Sig F | 0.0000 | | | |

| Factor | Name | Low | High | Exper |
|--------|----------|-----|------|-------|
| | | | | |
| | | | | |
| А | Supplier | 1 | 3 | 2 |
| В | Temp | 100 | 200 | 150 |
| С | Pressure | 50 | 80 | 65 |

| Multiple Response Prediction | | | | | | |
|------------------------------|---------|--------|-------------|---------------|--|--|
| | | | 99% Confide | ence Interval | | |
| | Y-hat | S-hat | Lower Bound | Upper Bound | | |
| Mixing Time | 19.8272 | 0.5843 | 18.074 | 21.580 | | |

| hat Model | | Mixing Time | • | | ive |
|-----------|---|--|-----------|-----|-----|
| Factor | Name | Coeff | P(2 Tail) | Tol | Act |
| Const | | 0.58425 | 0.0000 | | |
| | R ² Adj R ² Std Error F Sig F F _{LOF} Sig F _{LOF} | 0.0000 0.0000 0.0359 NA NA NA | | | |
| | Source | SS | df | MS | |
| | Regression | 0.0 | 0 | NA | |

Y bar Marginal Means Plot of Mixing Time





KISS Guidelines for Choosing and Experimental Design



NOTE 1: Sample size (n_{reps}) is for 95% confidence in \hat{s} and 99.99% confidence in \hat{y} .

NOTE 2: $(n_{reps}/2)$ will provide 75% confidence in \hat{s} and 95% confidence in \hat{y} .

NOTE 3: The 12 Run Plackett-Burman or L12 is very sensitive to large numbers of interactions. If this is the case, you would be better off using the 16 Run Fractional Factorial or a smaller number of variables in 2 or more full factorial experiments.

NOTE 4: For more complete 2-level design options, see next page.



Three Level Screening Design – L₁₈

OBJECTIVE: To test an orthogonal subset of the full factorial.

ADVANTAGES: Can screen many factors with just a few runs. Can estimate all main effects and all quadratics independently, as well as the AB interaction. Can mix qualitative and quantitative factors. Can handle up to seven three level factors.

DISADVANTAGES: No direct modeling of interactions

| | | | | | L ₁ | ₈ Desi | gn | | | | |
|-----|----|----|----|----|----------------|-------------------|----|----|---|---|---|
| Run | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | y ₁ y ₄ | ÿ | s |
| 1 | -1 | -1 | -1 | -1 | -1 | -1 | -1 | -1 | | | |
| 2 | -1 | -1 | 0 | 0 | 0 | 0 | 0 | 0 | | | |
| 3 | -1 | -1 | +1 | +1 | +1 | +1 | +1 | +1 | | | |
| 4 | -1 | 0 | -1 | -1 | 0 | 0 | +1 | +1 | | | |
| 5 | -1 | 0 | 0 | 0 | +1 | +1 | -1 | -1 | | | |
| 6 | -1 | 0 | +1 | +1 | -1 | -1 | 0 | 0 | | | |
| 7 | -1 | +1 | -1 | 0 | -1 | +1 | 0 | +1 | | | |
| 8 | -1 | +1 | 0 | +1 | 0 | -1 | +1 | -1 | | | |
| 9 | -1 | +1 | +1 | -1 | +1 | 0 | -1 | 0 | | | |
| 10 | +1 | -1 | -1 | +1 | +1 | 0 | 0 | -1 | | | |
| 11 | +1 | -1 | 0 | -1 | -1 | +1 | +1 | 0 | | | |
| 12 | +1 | -1 | +1 | 0 | 0 | -1 | -1 | +1 | | | |
| 13 | +1 | 0 | -1 | 0 | +1 | -1 | +1 | 0 | | | |
| 14 | +1 | 0 | 0 | +1 | -1 | 0 | -1 | +1 | | | |
| 15 | +1 | 0 | +1 | -1 | 0 | +1 | 0 | -1 | | | |
| 16 | +1 | +1 | -1 | +1 | 0 | +1 | -1 | 0 | | | |
| 17 | +1 | +1 | 0 | -1 | +1 | -1 | 0 | +1 | | | |
| 18 | +1 | +1 | +1 | 0 | -1 | 0 | +1 | -1 | | | |



L₁₈ Screening Design Example





L₁₈ Screening Design Example (cont.)

DOE PRO XL > Analyze Design > Marginal Means Plot...









L₁₈ Screening Design Example (cont.)

DOE PRO XL > Analyze Design > Multiple Response Regression

| Y-hat Model | | Dispense Vol | | | |
|-------------|---|---|-----------|-----|--------|
| Factor | Name | Coeff | P(2 Tail) | Tol | Active |
| Const | | 97.650 | 0.0000 | | |
| Α | X1 | -0.08056 | 0.2199 | 1 | Х |
| В | X2 | 0.27500 | 0.0011 | 1 | Х |
| С | X3 | 0.43958 | 0.0000 | 1 | Х |
| D | X4 | -0.74583 | 0.0000 | 1 | Х |
| E | X5 | 0.69167 | 0.0000 | 1 | Х |
| F | X6 | 0.64167 | 0.0000 | 1 | Х |
| G | X7 | 0.08542 | 0.2874 | 1 | Х |
| Н | X8 | -0.57500 | 0.0000 | 1 | Х |
| AB | | 0.78333 | 0.0000 | 1 | Х |
| BB | | 0.62500 | 0.0000 | 1 | Х |
| CC | | -1.256 | 0.0000 | 1 | Х |
| DD | | 2.175 | 0.0000 | 1 | Х |
| EE | | 0.02500 | 0.8566 | 1 | Х |
| FF | | 1.163 | 0.0000 | 1 | Х |
| GG | | 2.556 | 0.0000 | 1 | Х |
| HH | | 0.05000 | 0.7179 | 1 | Х |
| | R ² Adj R ² Std Error F Sig F | 0.9559 0.9431 0.5508 74.5448 0.0000 | | | |

| | | | | - |
|--------|------|-----|------|-------|
| Factor | Name | LOW | High | Exper |
| | | | | |
| | | | | |
| Α | X1 | -1 | 1 | 0 |
| В | X2 | -1 | 1 | 0 |
| С | Х3 | -1 | 1 | 0 |
| D | X4 | -1 | 1 | 0 |
| E | X5 | -1 | 1 | 0 |
| F | X6 | -1 | 1 | 0 |
| G | X7 | -1 | 1 | 0 |
| Н | X8 | -1 | 1 | 0 |
| | | | | |

| | Multipl | e Respons | e Prediction | |
|--------------|---------|-----------|--------------|--------------|
| | | | 99% Confide | nce Interval |
| | Y-hat | S-hat | Lower Bound | Upper Bound |
| Dispense Vol | 97.6500 | 0.4533 | 96.290 | 99.010 |

| | S-hat Model | | | | | | |
|---|-------------|--------------------|--------------|-----------|-----|------|--|
| | | | Dispense Vol | | | | |
| | | | | | | live | |
| | Factor | Name | Coeff | P(2 Tail) | Tol | Act | |
| | Const | | 0.45331 | 0.1238 | | | |
| С | Α | X1 | 0.28003 | 0.0523 | 1 | Х | |
| С | в | X2 | 0.04298 | 0.3701 | 1 | Х | |
| С | C | X3 | -0.03638 | 0.4203 | 1 | Х | |
| С | D | X4 | -0.03054 | 0.4752 | 1 | Х | |
| С | E | X5 | 0.09167 | 0.1903 | 1 | Х | |
| С | F | X6 | -0.07645 | 0.2253 | 1 | Х | |
| С | G | X7 | 0.09846 | 0.1779 | 1 | Х | |
| С | Н | X8 | 0.02019 | 0.6049 | 1 | Х | |
| | AB | | 0.09812 | 0.1784 | 1 | Х | |
| | BB | | 0.05088 | 0.4875 | 1 | Х | |
| | CC | | 0.03490 | 0.6055 | 1 | Х | |
| | DD | | -0.14938 | 0.2015 | 1 | Х | |
| | EE | | 0.00427 | 0.9445 | 1 | Х | |
| | FF | | 0.08219 | 0.3418 | 1 | Х | |
| | GG | | 0.02786 | 0.6705 | 1 | Х | |
| | HH | | -0.06678 | 0.4025 | 1 | Х | |
| | | | | | | | |
| | | R ² | 0.9953 | | | | |
| | | Adj R ² | 0.9199 | | | | |
| | | Std Error | 0.0978 | | | | |
| | | F | 13.1950 | | | | |
| | | Sig F | 0.2134 | | | | |



KISS Guidelines for Choosing and Experimental Design



NOTE 1: Sample size (n_{reps}) is for 95% confidence in \hat{a} and 99.99% confidence in \hat{y} NOTE 2: $(n_{reps}/2)$ will provide 75% confidence in \hat{a} and 95% confidence in \hat{y}

NOTE 3: The 12 Run Plackett-Burman or L12 is very sensitive to large numbers of interactions. If this is the case, you would be better off using the 16 Run Fractional Factorial or a smaller number of variables in 2 or more full factorial experiments.

NOTE 4: For more complete 2-level design options, see next page.



Response Surface Modeling Designs

OBJECTIVE: To test a <u>nearly orthogonal subset of the full factorial</u> in order to build a non-linear model for quantitative input factors (X's).



Box - Behnken Design Space



Central Composite Design (CCD) Space



Central Composite Face Design Space



Response Surface Modeling Designs Box - Behnken Designs

- **OBJECTIVE:** To test a nearly orthogonal subset of the full factorial in order to build a non-linear model for quantitative input factors (X's).
- **ADVANTAGES:** Can evaluate all main and all quadratic effects as well as all 2-way interaction effects. Much more efficient than the full factorial designs!
- **DISADVANTAGES:** Requires quantitative factors. Not available for 2 factors and too many runs for $k \ge 5$. Therefore, use only for 3 or 4 quantitative factors as shown below.





| | | | 4 fa | actor | ſS | |
|-----|---|---|------|-------|-------------------------------|---|
| Run | Α | в | С | D | y ₁ y ₄ | s |
| 1 | - | - | 0 | 0 | | |
| 2 | - | + | 0 | 0 | | |
| 3 | + | - | 0 | 0 | | |
| 4 | + | + | 0 | 0 | | |
| 5 | 0 | 0 | - | - | | |
| 6 | 0 | 0 | - | + | | |
| 7 | 0 | 0 | + | - | | |
| 8 | 0 | 0 | + | + | | |
| 9 | 0 | 0 | 0 | 0 | | |
| 10 | - | 0 | 0 | - | | |
| 11 | - | 0 | 0 | + | | |
| 12 | + | 0 | 0 | - | | |
| 13 | + | 0 | 0 | + | | |
| 14 | 0 | - | - | 0 | | |
| 15 | 0 | - | + | 0 | | |
| 16 | 0 | + | - | 0 | | |
| 17 | 0 | + | + | 0 | | |
| 18 | 0 | 0 | 0 | 0 | | |
| 19 | - | 0 | - | 0 | | |
| 20 | - | 0 | + | 0 | | |
| 21 | + | 0 | - | 0 | | |
| 22 | + | 0 | + | 0 | | |
| 23 | 0 | - | 0 | - | | |
| 24 | 0 | - | 0 | + | | |
| 25 | 0 | + | 0 | - | | |
| 26 | 0 | + | 0 | + | | |
| 27 | 0 | 0 | 0 | 0 | | |

Box – Behnken Example



Box Behnken

Example

R&D Laboratory



- Goal was to achieve Y = 1350
- 1 rep (although not ideal) was taken due to cost
- Most expensive factor was C
- To be competitive, highest setting for C is 45

| 2001 | y | | · ···· | noopoi | IOC Duit |
|--------|----------|-----|--------|---|----------|
| Factor | Α | В | С | | |
| Row # | Α | В | С | Y1 | Y bar |
| 1 | 4.5 | 30 | 75 | 211 | 211 |
| 2 | 4.5 | 120 | 75 | 1332 | 1332 |
| 3 | 6.5 | 30 | 75 | <mark>959</mark> | 959 |
| 4 | 6.5 | 120 | 75 | <mark>1163</mark> | 1163 |
| 5 | 4.5 | 75 | 30 | <mark>697</mark> | 697 |
| 6 | 4.5 | 75 | 120 | 427 | 427 |
| 7 | 6.5 | 75 | 30 | 724 | 724 |
| 8 | 6.5 | 75 | 120 | <mark>396 396 396 396 396 396 396 396 396 396 </mark> | 396 |
| 9 | 5.5 | 30 | 30 | <mark>783</mark> | 783 |
| 10 | 5.5 | 30 | 120 | 275 | 275 |
| 11 | 5.5 | 120 | 30 | <mark>779</mark> | 779 |
| 12 | 5.5 | 120 | 120 | 1251 | 1251 |
| 13 | 5.5 | 75 | 75 | 1282 | 1282 |
| 14 | 5.5 | 75 | 75 | <mark>1339</mark> | 1339 |
| 15 | 5.5 | 75 | 75 | 1304 | 1304 |

Design Matrix with Response Data









First Regression Output

| Y-hat Model | | Signal | | | |
|-------------|---|---|-----------|--------|--------|
| Factor | Name | Coeff | P(2 Tail) | Tol | Active |
| A | A | 1308.33 71.875 | 0.2085 | 1 | X |
| В | В | 287.13 | 0.0022 | 1 | Х |
| С | С | -79.250 | 0.1724 | 1 | Х |
| AB | | -229.25 | 0.0226 | 1 | Х |
| AC | | -14.500 | 0.8450 | 1 | |
| BC | | 245.00 | 0.0177 | 1 | Х |
| AA | | -301.54 | 0.0092 | 0.9890 | Х |
| BB | | -90.542 | 0.2716 | 0.9890 | |
| CC | | -445.79 | 0.0017 | 0.9890 | X |
| | R ² Adj R ² Std Error F Sig F | 0.9570 0.8795 140.8513 12.3576 0.0064 | | | |

Final Regression Output

| Y-hat Model | | Signal | | | |
|-------------|--------------------|----------|-----------|--------|------|
| | | Jightan | | | tive |
| Factor | Name | Coeff | P(2 Tail) | Tol | Ac |
| Const | | 1252.62 | 0.0000 | | |
| А | А | 71.875 | 0.1798 | 1 | Х |
| В | В | 287.13 | 0.0006 | 1 | Х |
| С | С | -79.250 | 0.1444 | 1 | Х |
| AB | | -229.25 | 0.0121 | 1 | Х |
| BC | | 245.00 | 0.0088 | 1 | Х |
| AA | | -294.58 | 0.0042 | 0.9949 | Х |
| CC | | -438.83 | 0.0004 | 0.9949 | Х |
| | | | | | |
| | R ² | 0.9435 | | | |
| | Adj R ² | 0.8870 | | | |
| | Std Error | 136.4369 | | | |
| | F | 16.6944 | | | |
| | Sig F | 0.0007 | | | |



• Using Multiple Response Optimizer, is there a way to hit the target value (1350), while keeping factor C at or below 45?

| Response Signal | Remove Constraint |
|---|--|
| Model Type Optimization Target Value Y-hat = I 1350 | Settings To <u>W</u> orksheet <u>H</u> elp |





- The team tried several confirmation tests, within the range of the experimental settings. Keeping C at 45, they confirmed that there was no way to hit their target value. Their predictions matched well with what DOE Pro predicted.
- The team then tried extrapolating with the settings for factor B. Since their prediction model worked well within their experimental range, they decided it was worth a shot to try something outside the range as suggested by their DOE model. Note that there is no guarantee that the model will extrapolate, so confirmation is especially critical!



| Factor | Name | Low | High | Eter |
|--------|------|-----|------|------|
| А | А | 4.5 | 6.5 | 5.23 |
| В | В | 30 | 120 | 143 |
| С | С | 30 | 120 | 45 |

| Multiple Response Prediction | | | | | | | | | |
|------------------------------|-----------|----------|-------------|---------------|--|--|--|--|--|
| 00% Confidence Interval | | | | | | | | | |
| | | | 99% Confide | ence Interval | | | | | |
| | Y-hat | S-hat | Lower Bound | Upper Bound | | | | | |
| Signal | 1350.1306 | 136.4369 | 940.820 | 1759.441 | | | | | |
| | | | | | | | | | |



Response Surface Modeling Designs Central Composite Designs (CCD)

- **OBJECTIVE:** To test a nearly orthogonal subset of the full factorial in order to build a non-linear model for quantitative input factors (X's).
- **ADVANTAGES:** Can evaluate all main and all quadratic effects as well as selected interactions (2-way and higher). Can be run sequentially: the 2-level part first and then test for linearity. If linear, no need to go further. If not, must add on axial points.

DISADVANTAGES: Primarily for quantitative factors.





Central Composite Designs Suggested Values for α and # of Center Points

- Face-centered Design ($\alpha = 1$)
 - Hard limits (restrictions) on factor settings
 - Cannot take factor settings beyond ±1 (coded values)
 - Predictions made within the "cube"
 - Recommended number of center points = 2
 - Orthogonality is worse with more than 2 center points
- Spherical Design ($\alpha = \sqrt{k}$)
- Rotatable Design ($\alpha = (n_F)^{1/4}$)
 - k is the number of factors; n_F is the number of runs in the factorial part of the design
 - No hard limits (constraints) on factor settings
 - Able to go beyond ±1 coded settings
 - Predictions slightly beyond the "cube" (in case the optimum lies just outside)
 - Orthogonality improves with more center points; 3-6 is recommended









2 Factor - CCD Template from DOE PRO XL

| | Run | pul | l back | stop | angle | Y1 | Y2 | Y3 | Y4 |
|-----------|-----|-----|--------|------|-------|----|----|----|----|
| Factorial | 1 | - | 160 | - | 2 | | | | |
| | 2 | - | 160 | + | 4 | | | | |
| | 3 | + | 180 | - | 2 | | | | |
| | 4 | + | 180 | + | 4 | | | | |
| Contor | 5 | 0 | 170 | 0 | 3 | | | | |
| Center | 6 | 0 | 170 | 0 | 3 | | | | |
| | 7 | - | 160 | 0 | 3 | | | | |
| Avial | 8 | + | 180 | 0 | 3 | | | | |
| Axiai | 9 | 0 | 170 | - | 2 | | | | |
| | 10 | 0 | 170 | + | 4 | | | | |





• Collect data and complete the factorial portion of the CCD.

| Factor | A | В | Distance | | | | | | | |
|--------|----------------|------------|----------|----|------|----|------|----|---------|----------|
| Row # | pullback angle | stop angle | Y1 | Y2 | | Y3 | | Y4 | Y bar | S |
| 1 | 160 | 2 | 27.5 | | 27.5 | | 27.5 | 27 | 27.375 | 0.25 |
| 2 | 160 | 4 | 47 | | 47 | | 48 | 48 | 47.5 | 0.57735 |
| 3 | 180 | 2 | 64.5 | | 64 | | 63.5 | 62 | 63.5 | 1.080123 |
| 4 | 180 | 4 | 77 | | 74 | | 75.5 | 75 | 75.375 | 1.25 |
| 5 | 170 | 3 | | | | | | | #DIV/0! | #DIV/0! |
| 6 | 170 | 3 | | | | | | | #DIV/0! | #DIV/0! |
| 7 | 160 | 3 | | | | | | | #DIV/0! | #DIV/0! |
| 8 | 180 | 3 | | | | | | | #DIV/0! | #DIV/0! |
| 9 | 170 | 2 | | | | | | | #DIV/0! | #DIV/0! |
| 10 | 170 | 4 | | | | | | | #DIV/0! | #DIV/0! |
| | | | | | | | | | | |

• Select Analyze Design from DOE PRO XL with only this data and duplicate the regression output on the next page!





- Row five data at the centerpoints is: 57, 57.5, 57, 57!
- Did not confirm! We need to collect the remaining rows of the CCD design (the Center and Axial portions of the design)!



• Collect the remaining data and complete the CCD design.





| Factor | | A | В | Distance | | | | | |
|--------|----|----------------|------------|----------|------|------|------|--------|----------|
| Row # | | pullback angle | stop angle | Y1 | Y2 | Y3 | Y4 | Y bar | S |
| | 1 | 160 | 2 | 27.5 | 27.5 | 27.5 | 27 | 27.375 | 0.25 |
| | 2 | 160 | 4 | 47 | 47 | 48 | 48 | 47.5 | 0.57735 |
| | 3 | 180 | 2 | 64.5 | 64 | 63.5 | 62 | 63.5 | 1.080123 |
| | 4 | 180 | 4 | 77 | 74 | 75.5 | 75 | 75.375 | 1.25 |
| | 5 | 170 | 3 | 57 | 57.5 | 57 | 57 | 57.125 | 0.25 |
| | 6 | 170 | 3 | 57.5 | 57 | 56.5 | 57 | 57 | 0.408248 |
| | 7 | 160 | 3 | 48 | 47 | 47 | 47 | 47.25 | 0.5 |
| | 8 | 180 | 3 | 73.5 | 75 | 73 | 74.5 | 74 | 0.912871 |
| | 9 | 170 | 2 | 43 | 42 | 42 | 42 | 42.25 | 0.5 |
| | 10 | 170 | 4 | 58 | 58 | 61 | 58.5 | 58.875 | 1.436141 |
| | | | | | | | | | |

 Select Analyze Design from DOE PRO XL with the complete data set and duplicate the regression output on the next page!





• One final regression to clean up the insignificant terms!



| Y-hat Mode | el la | | | | | | | | | | - | S-hat Model | | | | |
|------------|---|----------|-----------|-----------|------------|---------|-------------|-----------------|------------|-----------------|-----|-------------|----------------------|----------|----------|------------------|
| | | Distance | | | | Facto | r Name | Low | High | Exper | | | | Distance | _ | |
| | | | | | i <u>č</u> | | | | | | | | | | | <u>š</u> |
| Factor | Name | Coeff | P(2 Tail) | Tol | Act | | | | | | | Factor | Name | Coeff | P(2 Tail |) Tol 🛱 |
| Const | | 57.259 | 0.0000 | | | A | pullback an | igle 160 | 180 | 170 | | Const | | 0.71647 | 0.0002 | |
| А | pullback angle | 15.125 | 0.0000 | 1 | X | В | stop angl | e 2 | 4 | 3 | C C | А | pullback angle | 0.31927 | 0.0584 | 1 <mark>X</mark> |
| В | stop angle | 8.104 | 0.0000 | 1 | X | | | | | | - | | _ | | | |
| AB | | -2.063 | 0.0000 | 1 | X | | | | | | _ | | R ² | 0.3783 | | |
| AA | | 3.170 | 0.0000 | 0.9722 | Х | | Μι | Itiple Response | Prediction | | | | Adj R ² | 0.3006 | | |
| BB | | -6.893 | 0.0000 | 0.9722 | X | | | | | | | | Std Error | 0.3544 | | |
| | _ | | | | | | | | 99% Confi | idence Interval | | | F | 4.8684 | | |
| | R ² | 0.9924 | | | | | Y-hat | S-hat | Lower Boun | d Upper Bound | | | Sig F | 0.0584 | | |
| | Adj R ² | 0.9912 | | | | Distanc | e 57.2589 | 0.7165 | 55.110 | 59.408 | | | FLOF | 0.2207 | | |
| | Std Error | 1.3132 | | \square | | | | | | | • | | Sig F _{LOF} | 0.6528 | | |
| | F | 883.4346 | ; | | | | | | | | | | | | | |
| | Sig F | 0.0000 | | | | | | | | | | | Source | SS | df | MS |

• We now have a non-linear model for Y-hat and a potential linear model for S-hat! If the customer gives us a target, we now will be able to determine input settings to hit the target consistently! The target is 52 with a lower specification of 50 and an upper specification of 54. What are the input settings to hit this target consistently?



| Multiple Response | Optimizer (St | ep 1 of 3) | | > | | | | | | | |
|--|--|------------|--------------|---|--|--|--|--|--|--|--|
| Multiple Response | Multiple Response Optimization Step #1: <u>O</u> K | | | | | | | | | | |
| For each factor enter the low, high, and continuous information. | | | | | | | | | | | |
| Name | Low | High | <u>H</u> elp | | | | | | | | |
| pullback angle | pullback angle 160 180 🗹 Continuous | | | | | | | | | | |
| stop angle 2 4 Continuous | | | | | | | | | | | |

| Multiple Response (| \times | | | | | | | | | | |
|--|--|-----|--------------------|--------------|--|--|--|--|--|--|--|
| Multiple Response Op You may enable Cpk o USL blank, it will be co | Multiple Response Optimization Step #2 (Optional): You may enable Cpk optimization for each response and define the LSL and USL. If you leave LSL or USL blank, it will be considered a one sided limit. | | | | | | | | | | |
| | <u>C</u> ancel | | | | | | | | | | |
| Response | LSL | USL | S Estimate | <u>H</u> elp | | | | | | | |
| Distance | 50 | 54 | S Model (if Avail) | Cpk Enabled | | | | | | | |

| Multiple Response Optim | nizer (Step 3 of 3) - Co | onstraint Editor | | \times |
|--|--------------------------|------------------|-----------------------------|------------------------------|
| Current Constraints and A | nswers | | | |
| Distance: Max Cpk Weig | ght=50 RESULT = 1.252 | (50 of 50) | | ^ |
| Constraint Definitions Response | Distance | | <u>R</u> emo <u>O</u> pt | ve Constraint imize Again |
| Cpk Max = 1 | .251538147 ~ | 50 Veight | Setting | s To <u>W</u> orksheet |
| | <u>A</u> dd Constraint | | <u>H</u> elp | <u>C</u> ancel |
| Optimal Input Settings | | | | |
| pullback angle = 164.24228 stop angle = 4 | 487344 | | | ~ ~ |

| Factor | Name | Low | High | Exper |
|--------|----------------|-----|------|-------------|
| A | pullback angle | 160 | 180 | 164.2422849 |
| В | stop angle | 2 | 4 | 4 |

| Multiple Response Prediction | | | | | | | | | |
|------------------------------|-------------------------|--------|-------------|-------------|--|--|--|--|--|
| | 99% Confidence Interval | | | | | | | | |
| | Y-hat | S-hat | Lower Bound | Upper Bound | | | | | |
| Distance | 52.0000 | 0.5326 | 50.402 | 53.598 | | | | | |



KISS Guidelines for Choosing an Experimental Design



NOTE 1: Sample size (n_{reps}) is for 95% confidence in \hat{s} and 99.99% confidence in \hat{y} .

NOTE 2: $(n_{reps}/2)$ will provide 75% confidence in \hat{s} and 95% confidence in \hat{y} .

NOTE 3: The 12 Run Plackett-Burman or L12 is very sensitive to large numbers of interactions. If this is the case, you would be better off using the 16 Run Fractional Factorial or a smaller number of variables in 2 or more full factorial experiments.

NOTE 4: For more complete 2-level design options, see next page.



Key Takeaways



• As a review techniques, stop the video and summarize the key learnings from this session. When you are finished, continue to the next page.



Key Takeaways

- Full Factorial designs are great for mixed factors (at least one qualitative input factor) when K (number of factors) is 3 or less!
- The L₁₈ is a great screening design for mixed factors and larger K!
- The marginal means plots are used extensively with the full factorial and L₁₈ design when some of the factors are qualitative.
- Models do not make sense for qualitative input factors.
- The Box-Behnken and CCD designs are more efficient than the full factorial designs. For quantitative input factors only (typically K = 5 or less, these designs are perfect for model building with considerable less resources!
- The CCD design can be run sequentially. Keep it simple statistically (KISS) stay linear (two-level input factors) until shown otherwise. The center section is the confirmation of the linear model. If it confirms, congrats, you are complete (resources savings)! If it does not confirm, collect the center and axial pieces. Combine with the factorial piece and build the non-linear model.
- DOE PRO XL is nice software that has good graphical and optimization tools!



Supplemental Material



- Suggested Reading:
 - Lean Six Sigma: A Tools Guide by Adams, Kiemele, Pollock and Quan (pp. 139 146)
 - Basic Statistics Tools for Continuous Improvement by Kiemele, Schmidt and Berdine, 4th edition (Chapter 8)
 - Design for Six Sigma: The Tool Guide for Practitioners by Reagan and Kiemele (section 7.9)
 - Understanding Industrial Designed Experiments by Schmidt and Launsby (chapter 2, 3, and 5)
 - Air Academy's app: Six Sigma Quick Tools



- SPC XL[™] software training tutorials:
 - <u>https://airacad.com/our-insights/training-videos/spc-xl/</u>
- The data files for this session can be downloaded from the site where you are accessing this course.



Additional Practice / Review Questions



- For each of the following scenarios, identify the design (and corresponding sample size) you would recommend:
 - You have just completed a screening experiment and determined there are three critical factors in a process under study. All of the factors are quantitative and you suspect nonlinearities and several significant two factor interactions. You'd like to be able to build a nonlinear model.
 - You are studying a fairly new injection molding process. You and your team have identified a total of 5 potentially important factors to study. The factors are: a) material vendor; b) holding time; c) holding pressure; d) gate size; and e) mold temperature. You'd like to determine which of these five factors has the most significant effect on percent shrinkage for further investigation.
 - You want to study three factors in a process to determine a good combination for giving optimum performance. One of the factors (brand) is qualitative, and the other two are quantitative (time and temperature). You suspect nonlinearities and interactions amongst the factors.
 - You want to study three input factors in a chemical process to optimize the input factors for best performance. All of the input factors are quantitative. You are not sure of nonlinearities for the ranges of the input factors selected. You do suspect interactions amongst the input factors.



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